

AMENDMENT TO THE SPECIFICATION

Change paragraphs 0007 and 0008, as follows:

[0007] wherein α is ~~an~~ a mean linear expansion coefficient, E is Young's modulus, and σ is Poisson's ratio. The equation shows that the compressive stress F is increased by the increase of α and E.

B1 [0008] Conventionally, the float glass plate employed for the window glass of the vehicle has a thickness from 3.5 to 4.8 mm. Recently, there ~~have~~ has been strong demand to reduce the thickness of the window glass so as to decrease fuel cost by lightening the vehicle. However, assuming the area of the glass is the same, the glass is reduced in the heat capacity as the glass becomes thin, thus decreasing $(\Delta Q)_{\max}$. As a result, the surface compressive stress F decreases. Therefore, some reinforced glasses are proposed so as to compensate for that.

Change paragraph 0017, as follows:

B2 [0017] In a glass composition for manufacturing transparent sheet glass which is disclosed in the PCT (Japanese phase) H8-500811, a total amount of oxides of alkaline earth metals is not greater than 10 wt.% to obtain permeability. However, the amount ~~of amount~~ of oxides of alkaline metals is needed to be increased to keep viscosity, which reduces durability. Furthermore, particularly, in case of reinforcing a glass plate having a thickness of 3.1 mm or less, a sufficient compressive stress value can not be obtained.

Change paragraph 0035, as follows:

B3 [0035] When MgO is not smaller than 2%, sufficiently high thermal stress coefficient is hard to be obtained and furthermore, a liquidus temperature raises. The liquidus temperature raises also when CaO is less than 5% or more than 15%. Though SrO and BaO ~~is~~ are introduced in the glass in such a manner that SrO and BaO replace MgO and CaO, it is not desirable that the total amount of

B3 SrO and BaO exceeds 10 % because SrO and BaO are more expensive than MgO and CaO.

Change paragraph 0037, as follows:

B4 [0037] Li_2O , Na_2O and K_2O prompt the glass to melt, and a small amount thereof in the glass increases a thermal stress coefficient without lowering the durability of the glass. The efficiency of promotion of melting becomes poor when Na_2O is less than 10% or the total of Li_2O , Na_2O and K_2O is less than 10%, while the durability of the glass is lowered when Na_2O exceeds 18% or the total of Li_2O , Na_2O and K_2O exceeds 20%. Li_2O and K_2O ~~is~~ are preferable not to exceed 5% because they are more expensive than Na_2O .

Change paragraphs 0041 and 0042, as follows:

B5 [0041] The glass including T- Fe_2O_3 in this range has such solar control performance as not greater than 60% of the solar energy transmittance and not greater than 30% of the ultraviolet transmittance defined by ISO at a ~~either 1-6mm~~ thickness of 1-6 mm. T- Fe_2O_3 of less than 0.4% will reduce the ultraviolet and infrared absorptivity of the glass.

[0042] The glass containing T- Fe_2O_3 of greater than 1.9%, when it is melted in a glass melting furnace, absorbs a lot of radiant heat from a flame at the upper surface of the melted glass, so that the glass near the bottom of the melting furnace is ~~no~~ not heated enough. More than 1.9% T- Fe_2O_3 also makes the specific gravity of the glass too large.

Change paragraph 0051, as follows:

B6 [0051] As the glass has the larger thermal stress coefficient defined by the product of the mean linear expansion coefficient and Young's modulus, the glass will have the larger reinforcing capacity by air blast cooling. When the thermal stress coefficient of the glass having ~~either 1.8-5.0mm~~ a thickness of 1.8-5.0 mm is not less than 0.71 MPa/°C, the glass can keep the same surface

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Cont compressive stress as a conventional glass for vehicles. Although high Young's modulus is needed for the thermal stress coefficient since the mean linear expansion coefficient suited to production has an upper limit, glasses have hardly a very high Young's modulus. The upper limit of the thermal stress coefficient will be not greater than 0.90 MPa/°C.

Change paragraph 0055, as follows:

B7 [0055] Tables 1 to 5 show glass compositions and physical properties of Examples of the present invention, and Table 6 shows glass compositions and physical properties of Comparative Examples. In Table 1 to 6, α shows a mean linear expansion coefficient in a range from 50-350°C, ρ shows density of the glass, E shows Young's modulus, $\alpha \cdot E$ shows a thermal stress coefficient, d shows a thickness of the glass, YA shows a visible light transmittance measured by the C.I.E. illuminant A, TG shows a solar energy transmittance, and Tuv shows an ultraviolet transmittance defined by ISO. All ~~concentration~~ concentrations in Tables are expressed by weight percentage.

Change paragraph 0060, as follows:

B8 [0060] Examples 1-25 are glasses of which compositions are within the range of claim 1 and also within a range of claim 3. As shown clearly from Tables 1-5, each Example has the mean linear expansion coefficient within the range of claim 11 and the density within the range of claim 12. Among these Examples, Examples 1 and 5-25 have thermal stress coefficient within the range of claim 10 and are excellent in reinforcing capability. Examples 7-25 are glasses of which compositions are within the range of claim 2 which has more preferable range than claim 1.